MIRAMICHI SHORES PHASE 4 HYDROGEOLOGICAL REPORT PERMIT TO TAKE WATER TOWN OF SAUGEEN SHORES

Prepared for: Miramichi Shores Land Development Limited

January 2021

File 20007.00

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Miramichi Shores Land Development Limited c/o Brad Pryde 10 Collard Way, Box 1725 Port Elgin, Ontario N0H-2C0

Attention: Mr. Brad Pryde

Dear sirs:

Re: Miramichi Shores Phase 4 Residential Development Hydrogeological Report for a Permit To Take Water Town of Saugeen Shores File 20007.00

GAMAN Consultants Inc. is pleased to submit this hydrogeological report to support a Category 3 Permit To Take Water for the purpose of dewatering the shallow groundwater table at the subject site.

The work was initiated to assess the need for groundwater control measures to facilitate the installation of a perforated storm sewer. A Category 3 Permit To Take Water should be acquired from the Ministry of Environment, Climate and Parks (MECP). This hydrogeologic report should be submitted with the MECP Permit Application. We trust that this report satisfies your requirements.

Yours truly, GAMAN Consultants Inc.

Gog R Hentz

Gary R. Hendy, P.Eng. Consulting Engineer

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1.0 INTRODUCTION

1.1 BACKGROUND

This report provides the results of a hydrogeological assessment carried out by GAMAN Consultants Inc. (GAMAN) in support of an application by Miramichi Shores Land Development Inc. for a Category 3 Permit to Take Water (PTTW). The Permit application is required for temporary dewatering during construction and installation of underground services at Miramichi Shores Phase 4 residential development.

Miramichi Shores Phase 4 is a proposed estate residential development located on Part of Lots 55 and 56, Lake Range in the former Township of Saugeen, Town of Saugeen Shores, County of Bruce. The site is located north of the 10th Concession between Port Elgin and Southampton near the shores of Lake Huron. The regional location of the subject property is shown in Figure 1. The residential portion of the development is approximately 16.25 hectares in area. The proposed Plan of Subdivision comprises 14 residential lots shown in Figure 2.

Miramichi Shores Phase 4 will consist of partial services using municipal water and on-site subsurface sewage disposal (septic) systems. A perforated storm sewer system (PSS) will be installed along the road to control groundwater. The groundwater table is close to grade and there is an expectation that groundwater control measures will be needed to temporarily lower the water table to allow for the installation of the PSS beneath the road.

There have been other approved applications for temporary water taking permits near this site as described below:

Port Elgin Lakeside Woods Residential Development

Lakeside Woods was serviced in 2018 and home occupancy and construction continue. The development is located about 700 metres south of this site on the north side of Concession 10 and east of Miramichi Bay Road as shown in Figure 1. Groundwater control measures were needed to install underground services at the site under Permit To Take Water 7843-AZEL2T, dated July 18, 2018. The Permit allowed for dewatering at discharge rates up to 2,600,000 L/day. Dewatering reported no problems with calculated daily volumes ranging from 200,000 to 520,000 L/day.

Trunk Sanitary Sewer System and Sewage Pumping Station – 10th Concession

Positive groundwater control was required to lower the groundwater level for the construction of the trunk sanitary sewer and the sewage pumping station (located approximately 500 m from the proposed Lakeside Woods development). A hydrogeological assessment in support of an application for a PTTW for the construction dewatering associated with the trunk sanitary sewer and sewage pumping station was carried out by Henderson Paddon & Associates Limited (HPA), now part of WSP Canada Inc., on behalf of the Town of Saugeen Shores in 2008. The results of that assessment were provided to the Town in a report dated April 2008. The construction dewatering was subsequently carried out under PTTW 1077-7Q7P2X, issued to the Town of Saugeen Shores in March 2009. During the dewatering process, no reported problems were noted.

Summerside – Phases 1 to 4

Positive groundwater control was also required to lower the groundwater level for the construction of municipal services related to major residential development at the north end of Port Elgin south of the 10th Concession. A hydrogeological assessment in support of an application for a PTTW for construction dewatering associated with the installation of water mains, sanitary sewers and storm sewers was carried out by GENIVAR on behalf of the developer (Lord Elgin Estates Developments Limited) in 2012. PTTW 2511-8TNL3C was issued on April 26, 2012. A renewal of the water taking permit was required in 2016. WSP Canada on behalf of the developer made a subsequent application and PTTW 7758-AEFQAV was issued. There were no reported problems related to dewatering at the Summerside site.

Based on the results of geotechnical investigations for this proposed residential development and the previous hydrogeological assessments for construction projects in the study area, it is anticipated that positive groundwater control will be required to temporarily lower the water table to facilitate the installation of the underground services.

1.2 STUDY OBJECTIVES

The Province, under the Ontario Water Resources Act, regulates the use of groundwater. In 2016, the MECP introduced the Environmental Activity and Sector Registry (EASR) to streamline the requirements for an Environmental Compliance Approval (ECA) or a PTTW. For construction site dewatering, water takings must be less than 400,000 L/day under normal circumstances which exclude heavy rainfall to qualify for the streamlined EASR. If the water taking is expected to exceed 400,000 L/day, the applicant is required to follow the PTTW process.

The installation of the PSS is scheduled to commence later this year or during the summer of 2022. This hydrogeological assessment was prepared to evaluate the need for an EASR application or a PTTW application and then prepare the appropriate documentation to support this water taking.

1.3 STUDY METHODOLOGY

The study methodology for this work program was comprised of reviewing background information about the site and relying on soil and groundwater data provided by other project team members to understand and interpret subsurface conditions at the site. GAMAN completed in-situ hydraulic conductivity tests on groundwater monitors at the site and the data was interpreted as input to an assessment of dewatering volumes that ultimately determines the need for a PTTW or the streamlined EASR. Given that the result of this work showed the need to follow the PTTW process, additional documentation was prepared on surrounding groundwater users and potential effects from dewatering.

The tasks required to complete the work program included:

- Background review of the physical setting of the site including physiography, surficial geology and groundwater.
- Review of soil and groundwater data completed by others during the installation of 4 groundwater monitors and a drive point.
- > A site inspection of the site and surrounding area.

- > A review of local water well records and existing services around the site.
- Analysis of in-situ hydraulic conductivity tests to assess groundwater control measures.
- > Assessment of effects to nearby receptors.
- Preparation of a hydrogeological report to support a Category 3 Permit To Take Water Application.

This report documents the study findings of these investigations.

2.0 PHYSICAL SETTING

2.1 PHYSIOGRAPHY, SURFICIAL GEOLOGY AND DRAINAGE

Bruce County is covered by seven (7) physiographic regions. The study area and site are located within the Huron Fringe physiographic region as described by Chapman and Putnam (1984). This physiographic region is a narrow ridge of land extending along Lake Huron from Sarnia to Tobermory and consists of wave-cut terraces formed from glacial Lake Algonquin and glacial Lake Nipissing. Across the mouth of the Saugeen River and valley at Southampton, north of this development, glacial Lake Algonquin built a massive beach deposit.

The sand plains within this physiographic region are comprised of coarse textured glaciolacustrine sediments. Figure 3 illustrates the surficial geology within the Saugeen Valley Watershed with the approximate site location shown in the northwest area. The surficial geology illustrates the sand plain that extends over and beyond the study area.

The elevation of the tablelands east of the former Nipissing Bluff is above 194 masl. The ground surface at the toe of the bluff, east of the Site, is at an approximate elevation of 191 masl. Numerous groundwater seeps are present at the base of the embankment that support

baseflow within unnamed tributaries in the study area. The seeps arise east of this development.

Within the proposed residential area, local topographic elevations range from 181 masl to 187 masl at the easterly property boundary. Ground surface contours at the Site are shown on the Draft Plan, Figure 2. Drainage at the site is comprised of a water course that conveys runoff to the west and discharges into Miramichi Bay.

The area is located within the Lake Fringe Sub-watershed of the Saugeen Valley Conservation Authority. Our review of the source water protection assessment report and maps for this area show that both groundwater and surface waters are located within areas classified as low stress potential.

2.2 HYDROGEOLOGY

The water well record database and observation wells drilled at the site were reviewed and interpreted to present the following understanding of hydrostratigraphic units beneath the site. Figure 4 illustrates the locations of local water wells. Water well records are presented in Table A-1.

There are three (3) main hydrostratigraphic units within the immediate area of the site as follows:

- > The Upper Aquifer
- > Aquitard
- Bedrock Aquifer

<u>The Upper Aquifer</u> is comprised of saturated sands and gravels that form the sand plains described in Section 2.1. There are few water wells documented in the MECP water well record database near the site and most show this thin aquifer. The upper aquifer south of

Concession 10 may be about 4.5 metres thick at MECP Well #1406082 and about 3.3 metres thick at MECP Well #1407481 near the site (see Figure 4 and Table A-1). These saturated sands were observed to be at least 4 metres thick at the site based on BH20-01. Flowing sands prevented the augers from advancing the boreholes deeper. Water wells terminating in the upper aquifer were usually completed as shallow dug wells.

The Aquitard appears to be comprised of heterogeneous mixtures of sandy-silt, silty-sand or clayey-silty soils as described in water well records. The aquitard is at least 30 metres thick based on MECP well record #1403490. Other water well records show the presence of these fine-grained sediments that comprise the aquitard and it appears that water well contractors extended wells down to bedrock near the site. The four boreholes drilled at the site were not deep enough to confirm the depth to the aquitard.

<u>The Bedrock Aquifer</u> was encountered at depths of or greater than 30 metres. Domestic wells extract groundwater from this aquifer which is overlain by the thick aquitard described above.

There is evidence of one or more deeper overburden aquifers at other well records reported in Table A-1. Water well MECP 1402111 at Miramichi Bay adjacent to the site report productive zones of groundwater supply.

2.3 GROUNDWATER MOVEMENT

The movement of groundwater is influenced by regional and local topographic feature, and drainage. The site is located adjacent to the shoreline of Lake Huron and it follows that shallow groundwater movement should be from east to west towards the lake at the regional scale.

Local groundwater movement is influenced by local topographic and drainage features. Groundwater levels monitored at four observation wells drilled at the site confirms the movement of shallow groundwater from west to east towards Lake Huron as expected. The average horizontal groundwater gradient from BH20-01 to BH20-04 was 0.0126 m/m and is the essentially the same as the horizontal gradient calculated at Lakeside Woods (Figure 1) to the south.

2.4 LOCAL WATER SUPPLIES

Within the area bounded by County Road 21 to the east, Concession 10 to the south, Lake Huron to the west and South Street in Southampton to the north, there are few reported water wells. Much of the area surrounding this site is serviced with municipal water including this proposed development.

Local water well records are appended to the report in Appendix A and illustrated in Figure 4. There are about 23 wells reported in the database as summarized in Table A-1. Six water wells appear in Figure 4 within about 500 metres of the site; however, the area is now serviced with municipal water. Most wells are drilled and extract groundwater from depths greater than the 2-metre excavation required for the perforated storm sewer. Test rates from productive wells range from 2 to 100 Igpm (9 to 454 L/min) with an average test rate of 16.6 Igpm (74 L/min). If we ignore the 100 Igpm test rate, the average test rate is still high for domestic use at 12 Igpm (54 L/min).

The water wells located between the lake and the site are situated within the municipally serviced area as confirmed with the water hydrants during our site inspection. Water wells may still exist but are likely to be used for non-drinking water purposes such as lawn watering.

The cluster of wells east of the site on Lot 54 includes well abandonment records for two wells (1407272 and 1407273). The two productive wells include a dug well and a shallow drilled well. These wells are located more than 500 metres from this development.

The wells in the area extract groundwater from thicker portions of the water table aquifer, deeper overburden aquifers or the bedrock aquifer. Groundwater is commonly reported as fresh in the water well record database. An exception is MECP well #1407421 north of the site that was drilled deep into bedrock (~100 metres) and encountered sulfurous water.

2.5 WATER BUDGET

As precipitation falls to the ground in the form of rainfall or snow, it is subject to components of the hydrological cycle. Water will generally runoff, infiltrate, evaporate or be subject to transpiration from plant uptake. Evaporation and transpiration are commonly grouped together as evapotranspiration while runoff and infiltration are grouped together as water surplus. The water budget is represented in a simple form as follows:

Water In = water Out P + EI = ET + IR + RO + EO

Where:

P = Precipitation

EI = External Inputs (Run-on, irrigation and vertical/lateral transfers)

ET = Evapotranspiration from plant uptake and evaporation.

IR = Infiltration Recharge

RO = Run-off

EO = External Outputs (water taking and vertical/lateral transfers)

Precipitation data is available from the Environment Canada website for climatic stations across the country. The Hanover Climatic Station provides climatic data temperature and precipitation for the period 1981 to 2010.

Thornthwaite (1948) developed a mathematical method for analyzing precipitation data and calculating evapotranspiration and water surplus. Average monthly temperature and precipitation data were analyzed using the method provided by Thornthwaite. The results are presented in Table 3 show the 30-year normal annual precipitation at 1,087 mm/yr. with a resultant water surplus of 505 mm/yr.

The MOECC Hydrogeological Technical Information Requirements For Land Development Applications (1995) included Table 2 derived from hydrologic analysis for assessing peak runoff for storm water management. The method considers topography, soil type and vegetation cover on the site as summarized in the table below.

Infiltration Factors	Range of Values	Assessment of Site	Selected Factor
Topography	0.1-0.3	Hilly	0.1
Soil Type	0.1-0.4	Open sandy loam	0.4
Cover	0.1-0.2	Woodland	0.2
Total Infiltration Factor			0.7

The rationale for selecting infiltration factors from this table is as follows:

- ➤ The infiltration factor for topography was estimated at 0.1 to reflects hilly topography.
- > The soil infiltration factor was estimated at 0.4 to reflect the sandy texture.
- > The cover factor of 0.2 reflects the woodlands.

The infiltration factor for this site is estimated at 0.70. The infiltration rate associated for the site is the product of the infiltration factor (0.70) and the water surplus (505 mm/yr.) and results in 354 mm/yr./ha.

3.0 SITE INVESTIGATIONS

CMT Engineering Inc. was retained by the developer to carry out geotechnical investigations. The firm completed a geotechnical investigation and documented the findings in a report titled "Geotechnical Investigations, Miramichi Shores Phase 4 Subdivision – Saugeen Shores dated January 2021. Four groundwater monitors were installed as part of the program and the borehole logs are included in Appendix B.

Soils beneath the site are comprised of sand fill overlying sand. Groundwater monitor details and water levels are detailed in Tables B-1(a) and B-1(b), Appendix B. The presence of these sands is consistent with other development sites in the area and with the physical setting of the broader area.

A drive point designated DP20-01 was installed below the creek bed near BH20-04. The purpose of the drive point was to provide an understanding of groundwater and surface water interaction to determine the potential effects of dewatering on surface water. Water levels in the drive point and the surface water level beside it are documented in Table B-1(b).

4.0 **DEWATERING ASSESSMENT**

4.1 DEWATERING CALCULATIONS

The dewatering requirements for the site were reviewed and assessed using the proposed depth of the perforated storm sewers (PSS), soil and groundwater conditions presented in the borehole logs completed by CMT Engineering Inc.

We understand that it is proposed to extend the PSS to a depth of 1.5 metres below proposed grade. There is about 250 metres of underground services to install from Carter Drive to the cul-de-sac.

Soil and groundwater conditions were evaluated below the site at four locations. Borehole logs for BH20-01, BH20-02, BH20-03 and BH20-04 (Appendix B) show that the upper aquifer is at least 4 metres thick. This is similar to the Lakeside Woods site along Concession 10 where the upper aquifer was documented at 4.1 metres thick.

Groundwater levels were monitored the boreholes on several occasions. The borehole construction details and water level elevations are documented in Table B-1, Appendix B. If the maximum depth of servicing is 1.5 metres below proposed grade, the water table may need to be lowered from about 0.8 to 1.2 metres based on water levels at boreholes BH20-01 and BH20-02, respectively. The water table may not need to be lowered at BH20-03.

In-situ rising head hydraulic conductivity (slug) tests were completed at the four boreholes. The data was analyzed using Aquifer Test Pro (Version 9.0) software and the results are presented in Figures C-1 to C-12, Appendix C. The test results for boreholes BH20-01 to BH20-04 reflect estimates of hydraulic conductivity ranging from 3.46×10^{-5} to 1.08×10^{-4} m/s with a geometric mean value of about 5.6×10^{-5} m/sec. Borehole BH20-01 provided the highest hydraulic conductivity at 1.08×10^{-4} m/sec.

Dewatering calculations at the site were evaluated based on the following assumptions:

- 1. The upper aquifer is up to 4 metres thick at the site.
- 2. The water table would be lowered by a maximum of 1.3 metres to facilitate the installation of perforated storm sewers up to 1.2 metres below the water table across the site.
- 3. Linear trenches 100 metres long by 2 metres wide would be dewatered at a time.

Powers presented a method for analyzing a long narrow system of dewatering that incorporates the flow from the sides (line source) and from radial flow from the ends of the dewatering system. Dewatering calculations presented in Tables D-1 and D-2, Appendix D reveal that daily volumes could range from an average of about 391,000 to a maximum of 558,000 L/day for hydraulic conductivities ranging from the average to the maximum values noted above, respectively. The zone of influence (Ro) ranges from about 30 to 40 metres. Dewatering rates at 391,000 L/day create the 30-metre zone of influence for underground services between BH20-02 and BH2-03. The higher volume of 558,000 L/day creating the 40-metre zone of influence reflects conditions between BH20-01 and BH20-02. The widths of dewatering (L) from the sides of the trench are about half the distance reported above. Figure 5 illustrates the 30-metre zone of influence that reflects the average hydraulic conductivity for the site.

We anticipate that the dewatering volumes would be lower in the northwest area of the site by BH20-03. As the excavation proceeds along Mary Rose Court, the aquifer becomes less transmissive based on the insitu hydraulic conductivity tests at BH20-02 to BH20-04. The length of dewatering may need to be adapted (shortened or lengthened) based on the volumes of water encountered and potential effects to nearby receptors.

4.2 ALLOWANCES FOR DEWATERING UNCERTAINTY

We have examined the results from dewatering at a nearby site that was serviced in 2018 to compare theoretical volumes from actual rates of dewatering to determine the need to adjust the volumes for uncertainty.

Lakeside Woods is a residential development comprised of 29 lots on a 6.1 ha parcel of land. The site is located about 700 metres south of this property in the same physical setting as this site. A Permit To Take Water #7843-AZEL2T, dated July 18, 2018 allowed for dewatering at discharge rates up to 2,600,000 L/day.

Soil and groundwater conditions at the Lakeside Woods site are similar to this site. The dewatering assessment at Lakeside Woods concluded that dewatering volumes could range from 245,000 to 405,000 L/day for soils with hydraulic conductivities up to 6.7×10^{-5} m/sec. Table D-4 summarized daily water takings from the dewatering system. Daily volumes of dewatering ranged from about 200,000 to 520,000 L/day. The observed volumes were within the estimated range from the theoretical evaluation except for the first four days of pumping where volumes were around 517,000 L/day and declined to 445,000 L/day. By day 5, volumes were below 400,000 L/day. From August 8 to August 30, 2018, the average daily water taking was calculated at 365,000 L/day and this is within the expected range calculated from the theoretical evaluation.

The uncertainty around these higher initial volumes may be due to one or a combination of the following:

- 1) The initial response and release of water from storage within an unconfined aquifer.
- 2) The linear trench may have exceeded the 100 metres assumed in the evaluation.
- 3) Locally higher hydraulic conductivities than observed from testing.
- 4) A thickening of the aquifer between boreholes.
- 5) Precipitation

The estimates of dewatering volumes in Tables D-1 and D-2 are based on hydraulic conductivity tests at each borehole and may not reflect variability in hydraulic conductivity. Table D-3 provides a sensitivity analysis for a scenario where the hydraulic conductivity increases by three times the maximum K value at BH20-01 to 3.24×10^{-4} m/sec. This scenario reveals that the water volumes could increase to about 1,047,000 L/day.

The zone of influence increases to 70 metres for this higher rate of dewatering. Dewatering at these high rates is not expected to be sustained by the aquifer based on the observed results at Lakeside Woods and lower hydraulic conductivities at other boreholes. The water budget for this site was presented in Section 2.5 and documented recharge at 70% of the water surplus or about 35% of the total precipitation. If a 50mm precipitation event occurred during dewatering, the additional volume of water that could be captured from this event includes the following:

- 1) The zone of influence comprises the recharge area.
- 2) All the recharge captured within the ZOI is removed by dewatering in one day.
- 3) The recharge area for the zone of influence extends 40 metres away from a 100 metre long dewatering system.
- 4) A 50-mm rainfall event is assumed to produce 17.5 mm of infiltration.

The volume of water captured by the dewatering system is the product of the zone of influence (180m x 80m) and 17.5 mm of recharge or 252 m³/day (252,000 L/day).

While we would not expect to see high volumes of pumping across the site, this scenario provides reason to increase the amount of water taking due to uncertainty. It is appropriate to undertake a Category 3 Permit To Take Water Application for dewatering up to 1,300,000 L/day to accommodate uncertainty in the hydraulic conductivity and rainfall.

There is about 250 metres of perforated storm sewers to install along the subdivision road and it should be possible to reduce the trench lengths to lower the volumes if needed. Servicing at this site is expected to last less than one month based on the results at Lakeside Woods.

4.3 DISCHARGE PLAN

Groundwater at this site flows towards and discharges to Lake Huron which is a short distance from the west property boundary. There is an unnamed water course that drains through a culvert beneath Miramichi Bay Road. It is proposed to discharge shallow groundwater to the tributary near BH20-4 (Figure 2) where it will flow directly into Lake Huron.

The discharge water will pass through appropriate siltation controls (e.g.: sedimentation tanks, rock check dams, silt bags, hay bales, splash pads, etc.) before it is conveyed to the roadside culvert.

4.4 **GROUNDWATER QUALITY**

Once the discharged water passes through the appropriate filtration system(s), it is expected that the level of total suspended solids (TSS) in the water will be low. Typically, discharge water from construction sites should contain no more than 25 mg/L of TSS. Periodic sampling will be needed to confirm TSS levels and ensure compliance with this criterion.

Tests for TSS are done by certified laboratories; however, the results are not available immediately. It is proposed to use field turbidity as a surrogate for TSS. Turbidity will be measured in the field and a corresponding sample of water will be sent to a certified laboratory for analysis of TSS. The field turbidity results will then be used to establish a relationship between TSS and turbidity so that remedial action, if needed, can occur sooner in the field. During the intervening time when the ratio of turbidity to TSS is established, the site should adopt a turbidity criterion up to 8 NTU as acceptable for TSS.

5.0 <u>RECEPTORS</u>

Several receptors were identified during the site inspection and from our review of other reports for this project noted in the references (Section 8) as follows:

- 1. Wells
- 2. Aquatic ecosystems.
- 3. Wetlands

Wells

Private water wells were discussed in this report. The area is serviced with municipal water and we are not aware of shallow dug wells in the area. It is assumed that other dwellings in the area are connected to the water works system. There may be some wells that have been retained perhaps for sprinklers or other uses by some residents. Water wells appear to extract groundwater from aquifers and depths below the shallow excavation levels proposed during this short period of dewatering.

Estimates of the predicted zones of influence (ZOI) presented in Section 4.1 ranges from about 30 to 40 metres from the ends of the dewatering system. The larger ZOI is expected in the vicinity of BH20-01 and BH20-02 where the soil conditions appear more transmissive. The lower ZOI is expected to result from dewatering between BH20-02 and BH20-03. The ZOI is expected to be closer to the lower range of this estimate if aquifer conditions do not change from the observed site conditions as described in Section 4.1. We infer that adverse effects to residents reliant on wells for drinking water are not anticipated. There appears to be a low risk of adverse effects to wells in the area from this temporary lowering of the water table.

Aquatic Ecosystems

WSP Canada Inc. completed an EIS for the subject lands. There is one water course at the site. The nearest distance from the storm sewer to the permanent water course is about 90 metres from the bulb at BH20-03 and is near BH20-04. Groundwater levels at BH20-04

and drive point DP20-01 beneath the water course show surface water levels are higher than groundwater levels at DP20-01 and BH20-04. The hydraulic head is downwards from surface water to groundwater and shows the water course loses water to the water table at that location.

The water course is about 1.4 metres wide and about 0.24 metres deep. The permanent water course could be influenced by temporary dewatering if aquifer conditions change beyond those observed at the four boreholes. It would be prudent to inspect and document conditions in this area during dewatering though the risk of an adverse effect seems low.

The zone of influence from dewatering in this area of the site was estimated at about 40 metres which should prevent the ZOI from extending to the water course, 90 metres away.

In summary, the proposal is to initiate dewatering at the site is not expected to affect the permanent water course. Groundwater and surface water levels should be monitored at BH20-04, DP20-01 and the water course to verify these observations.

Terrestrial Ecosystems

The WSP report noted documented sensitive areas across the site. Unmapped wetlands are designated Units 1 to 4 on Figure 4. Part of Unit 4 extends across lots 12-14. Dewatering at these high rates is temporary. Recharge from upland area should replenish the water table at the site. WSP considered the temporary affects from dewatering to not have an adverse impact on Unit 4.

6.0 ENVIRONMENTAL MANAGEMENT PLAN

Section 5 described the various potential receptors that could be affected by dewatering and concluded that the risk of adverse effects was low. Despite the low level of risk, it is proposed to initiate a groundwater monitoring program for the site.

Water levels at shallow observation wells designated BH20-01 to BH20-04, drive point DP20-01 and the water course should be monitored to document the effects of dewatering on the water table before, during and after dewatering. Water levels should be monitored at least three times before dewatering begins and then three times weekly during dewatering. Post construction monitoring would continue until groundwater levels rebound by 80% based on the baseline water levels.

If a water well supplying drinking water to a dwelling exists, a sample of groundwater will be collected for chemical analysis, provided the resident agrees to testing. Water quantity volumes should be documented daily and be retained on site for MECP inspections. The results will be submitted to the MECP as required under the PTTW.

Environmental inspections should occur during the dewatering period. The inspection should be completed to address the Conditions of the PTTW. The rates and taking of groundwater should be reviewed by the inspector and the discharge location examined for erosion related features caused by dewatering.

During the first 5-days of dewatering, TSS and Turbidity should be monitored daily to establish a ratio for turbidity and TSS going forward. Beyond the first 5-days, discharge water should be tested at least 3 times a week for field turbidity and one sample of water should be collected and tested by a certified laboratory for TSS weekly to continue correlating turbidity with TSS. If a turbidity value is observed to be higher than a concentration observed during the initial 5-days, a sample of this water should be tested for TSS to update the ratio of TSS to turbidity.

In the unlikely event that a resident who owns a water well experiences a water shortage, the complaint must be registered with the MECP within 24-hours of receiving the complaint. A temporary source of water should be provided to the dwelling within 24-hours if the well is a source of drinking water if the cause of water shortage is unclear or dewatering is known to be the cause. An investigation and report should be initiated into the cause of water shortages.

Water supply companies should be on standby in the event of a water shortage issue. The solution may be to provide bottled water for drinking and a water tank hookup until dewatering ceases and groundwater levels rebound by 80% at the site observation wells. A sample of groundwater should be collected and tested from a groundwater monitor at the site to establish baseline water quality. A grab sample of discharge water should be collected and tested every two weeks during dewatering to ensure ongoing compliance with surface water quality.

7.0 <u>CONCLUSIONS AND RECOMMENDATIONS</u>

The conclusions and recommendations presented below are premised on the data collected and reviewed at the site and existing information reviewed for this study:

- The study area and site are located within the Huron Fringe physiographic region. The sand plains within the region are comprised of coarse textured glaciolacustrine sediments.
- The Upper Aquifer (water table) is comprised of saturated sands and gravels that form the sand plains. The upper aquifer is about 4 metres thick based on local well record information.
- > The aquitard that underlies the water table is thick and comprised of low permeability till.

- Groundwater levels at the site range from about 0.7 to 1.3 metres below grade. Underground services to depths up to 1.5 metres below proposed grade necessitates the need to lower the water table up to 1.3 metres.
- Insitu hydraulic conductivity tests completed at four monitors shows the saturated sands to have an average value of 5.6x10⁻⁵ m/sec and a maximum value of 1.08x10⁻⁴ m/sec. These hydraulic conductivities are consistent with values determined at other sites in the study area.
- > Dewatering volumes ranging from 391,000 to 558,000 L/day may be observed.
- A sensitivity analysis to consider higher hydraulic conductivity and precipitation shows dewatering volumes could rise to 1,300,000 L/day.
- The interpreted zone of influence caused by dewatering ranges from 30 to 40 metres away from the well points.
- There are no reported adverse impacts on local domestic wells. Based on these observed and predicted effects, there continues to be a low risk of adverse effects to wells in the area from this temporary lowering of the water table.
- The developer should submit this report along with an Application for a Category 3 Permit To Take Water Application.

Respectfully Submitted, GAMAN CONSULTANTS INC.

Gog R Hentz

Gary R. Hendy, P.Eng. Consulting Engineer

8.0 LIMITATIONS AND USE

This report has been prepared for the exclusive use of Miramichi Shores Land Development Limited for their exclusive use in the evaluation of the area for the proposed development. GAMAN Consultants Inc. accepts no responsibility for any damages incurred by any third party resulting from decisions made, or actions taken based upon the information contained within this report.

All background information used in the preparation of this report has been relied upon in good faith, and GAMAN does not accept any responsibility for any misstatements, inaccuracies, or deficiencies contained in those documents or records. The information contained in this report should be evaluated, interpreted and implemented only in the context of the assignment.

The findings and conclusions included in this report reflect our best judgement in light of the information available at the time of report preparation and site inspection and are valid only at the date of issuance. If additional information is provided in the future, such as the results of additional site-specific assessments or monitoring, GAMAN will be pleased to re-evaluate our conclusions contained within this report, and issue amendments, as required.

9.0 <u>REFERENCES</u>

CMT Engineering, 2021

Geotechnical Investigations, Miramichi Shores Subdivision Phase 4

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Hydrogeological Assessment For Permit To Take Lakeside Woods Residential Development, Part Lot 51, Lake Range, Town of Saugeen Shores,

Chapman L.J. and Putnam, D.F., 1984

The Physiography of Southern Ontario, 3rd edition;

Ontario Geological Survey Special Volume 2; Ministry of Natural Resources.

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WSP, 2021

Environmental Impact Study, Mary Rose Subdivision, Saugeen Shores, Ontario

FIGURES



To Take Water For Miramichi Shores Land Development Limited							
Project:							
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GAMAN Consultants Inc.









APPENDICES

APPENDIX A

WATER WELL RECORDS

TABLE A-1 SUMMARY OF WATER WELL RECORDS

Miramichi Bay Phase 4 Permit To Take Water Evaluation (Project 20007.00)

TOWNSHIP CON LOT	UTM (metres)	DATE & Driller	CASING DIA (in)	WATER FOUND (ft)	Static Level (Ft.bgl)	Pumping Level (ft. bgl)	Test Rate (Igpm)	WELL USE	SCREEN top / Length	WELL ID	FORMATION (feet)
SAUGEEN TOWNSHIP LR 055	17 468974 4924189	1954/05 1705	4	FR 0141	2	6	10	PS		1402111 ()	MSND 0016 MSND GRVL 0035 HPAN STNS 0054 CLAY 0063 HPAN STNS 0136 MSND GRVL 0140 GRVL 0141
SAUGEEN TOWNSHIP LR 056	17 468874 4924449	1961/07 1804	4	FR 0142		80	2	DO		1402112 ()	GRVL STNS 0005 BLUE CLAY 0015 HPAN GRVL 0032 BRWN CLAY STNS 0090 MSND GRVL 0102 QSND 0129 FSND 0136 MSND GRVL 0140 GRVL 0142
SAUGEEN TOWNSHIP LR 046	17 467864 4922634	1968/04 1804	4	FR 0092 FR 0096	8	60	10	DO		1402163 ()	LOAM 0002 CLAY MSND BLDR 0030 CLAY MSND 0075 MSND GRVL 0092 GRVL 0096
SAUGEEN TOWNSHIP LR 057	17 469184 4924434	1972/05 5507	5	FR 0111	8	50	10	DO		1403067 ()	SAND 0020 BRWN CLAY 0108 GRVL 0113
SAUGEEN TOWNSHIP LR 047	17 467974 4922694	1973/10 2644	4	FR 0068	19		5	DO	0068 4	1403332 ()	CLAY 0002 BLDR CLAY 0020 CLAY SAND 0068 GRVL 0075 CLAY STNS 0093
SAUGEEN TOWNSHIP LR 051	17 468342 4923517	1974/02 5507	55	FR 0143	10	60	14	DO		1403490 ()	GRVL STNS 0010 CLAY GRVL STNS 0124 BLUE SHLE ROCK 0150
SAUGEEN TOWNSHIP LR 050	17 468220 4923328	1974/05 1804	5	FR 0141	18	40	15	DO		1403508 ()	BRWN STNS GRVL 0010 BRWN BLDR CLAY 0082 GREY SAND BLDR 0110 GREY GRVL SAND 0141
SAUGEEN TOWNSHIP LR 049	17 469890 4922064	1974/07 3408	7	FR 0040	10	17	10	DO	0038 4	1403591 ()	SAND CLAY 0026 SAND GRVL 0048
SAUGEEN TOWNSHIP LR 050	17 468164 4923424	1977/11 3030	36 30	FR 0005 FR 0015	15			DO		1404665 () A	BRWN LOAM 0001 BRWN GRVL 0005 BLUE CLAY STNS 0030
TABLE A-1 SUMMARY OF WATER WELL RECORDS

Miramichi Bay Phase 4 Permit To Take Water Evaluation (Project 20007.00)

TOWNSHIP CON LOT	UTM (metres)	DATE & Driller	CASING DIA (in)	WATER FOUND (ft)	Static Level (Ft.bgl)	Pumping Level (ft. bgl)	Test Rate (Igpm)	WELL USE	SCREEN top / Length	WELL ID	FORMATION (feet)
SAUGEEN TOWNSHIP LR 050	17 468214 4923424	1978/08 1737	55	FR 0141 FR 0156	50	82	3	DO		1404938 ()	SAND GRVL STNS 0006 BLUE CLAY GRVL STNS 0013 BLUE CLAY STNS SNDY 0045 SAND GRVL BLDR 0094 GREY HPAN STNS 0112 BRWN CLAY 0124 GREY HPAN STNS 0133 BRWN LMSN HARD DKCL 0135 BLUE LMSN 0137 BRWN LMSN SHLE LYRD 0141 GREY LMSN HARD DKCL 0156
SAUGEEN TOWNSHIP LR 048	17 468014 4922924	1978/10 1737	55	FR 0148 UK 0159	18	20	10	DO		1404959 ()	SAND FILL 0001 SAND 0003 GREY SAND 0006 SAND GRVL 0012 BLUE CLAY STNS 0038 BRWN CLAY 0055 GRVL CLAY 0074 QSND 0096 GREY HPAN STNS 0138 BLUE SHLE LMSN SOFT 0144 BRWN LMSN HARD 0160
SAUGEEN TOWNSHIP LR 047	17 467964 4922824	1979/12 1737	5	FR 0086	14	42	6	DO	0088 3	1405292 ()	CSND 0004 GREY SAND MARL CLAY 0007 BLUE CLAY STNS 0015 BLUE SAND GRVL CLAY 0042 GREY HPAN SNDY 0064 GREY HPAN STNS 0082 GRVL 0084 SAND GRVL 0090 FGVL 0091
SAUGEEN TOWNSHIP LR 046	17 468514 4922474	1981/07 4302	2	FR 0008	9	12	23	MN	0019 5	1406082 ()	BRWN CSND 0008 GREY MSND 0019 GREY SAND GRVL 0024 GREY CLAY SILT 0025
SAUGEEN TOWNSHIP LR 053	17 468880 4923717	1989/09 5507	5	SU 0425		425	25	DO		1407421 (25232)	CLAY SNDY 0016 CLAY BLDR 0141 BLUE SHLE ROCK LYRD 0425
SAUGEEN TOWNSHIP LR 054	17 469448 4923525	1990/01 1129	8	FR 0008	8	16	23	PS	0016 3	1407480 (54115)	BLCK LOAM 0001 BRWN SAND GRVL 0019 GREY CLAY SILT STNS 0020

TABLE A-1 SUMMARY OF WATER WELL RECORDS

Miramichi Bay Phase 4 Permit To Take Water Evaluation (Project 20007.00)

TOWNSHIP CON LOT	UTM (metres)	DATE & Driller	CASING DIA (in)	WATER FOUND (ft)	Static Level (Ft.bgl)	Pumping Level (ft. bgl)	Test Rate (Igpm)	WELL USE	SCREEN top / Length	WELL ID	FORMATION (feet)
SAUGEEN TOWNSHIP LR 055	17 469432 4923515	1990/01 1129	8	FR 0008	8	16	23	PS	0016 3	1407481 (54116)	BLCK LOAM 0001 BRWN SAND GRVL 0019 GREY CLAY SILT STNS 0020
SAUGEEN TOWNSHIP LR 051	17 468266 4923560	1990/10 1737	66	FR 0384		101	4	DO		1407721 (85519)	LOAM 0001 BRWN SAND STNS SOFT 0007 BRWN SAND CLAY STNS 0021 GREY CLAY STNS SOFT 0049 BRWN CLAY HARD 0091 GREY HPAN STNS HARD 0131 BLUE LMSN MGRD HARD 0197 BLUE LMSN DKCL HARD 0269 BRWN LMSN DKCL HARD 0305 BRWN LMSN MGRD HARD 0384
SAUGEEN TOWNSHIP LR 052	17 470278 4922798	1991/05 1737	6	FR 0032	8	11	20	DO	0029 3	1407876 (099603)	LOAM 0001 BRWN SAND GRVL SOFT 0006 GREY CLAY SILT SOFT 0017 GREY SAND SOFT 0032 GREY CLAY SILT SOFT 0044
SAUGEEN TOWNSHIP LR 052		1992/05 1737	6	FR 0016	4	8	15	со	0014 3	1408151 (114852)	BRWN SAND SOFT 0016 GREY SAND SOFT 0025 GREY SAND SILT SOFT 0027
SAUGEEN TOWNSHIP LR 048	17 468925 4922412	1995/05 6634	6	FR 0165 UK 0172	16	70	5	DO		1408770 (146801)	LOAM 0002 CLAY STNS 0018 CLAY SNDY 0086 CLAY SNDY STNS 0143 LMSN 0172
SAUGEEN TOWNSHIP LR 057	17 469959 4923980	1999/06 5507	6	FR 0320 FR 0490	49	495	100	DO		1409470 (202548)	SAND 0012 CLAY SOFT 0105 HPAN STNS 0182 SHLE STNS 0234 LMSN 0495
SAUGEEN TOWNSHIP 054	17 469439 4923487	2002/11 1129								1410272 (54229) A	
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H FLAUL	HAS THEET	FEET FEET	FEET FE	ET				TER	•
	GPM Rada	425 FEET 1 C		Y	pe)		Wr N	T	4
RECONMENDED PUNP	TYPE RECOMMEND PUMP DEEP SETTING	A3-45 RECOM	NG 5 4 GF	. W	ولل من			العلا	•
50-53					A way	Ā	1.to !	53/5	:4
FINAL STATUS	1 WATER SUPPLY 2 OBSERVATION W 3 TEST HOLE		D. INSUFFICIENT SUPPL D. POOR QUALITY ED		An C		Jak	y Ro	The
OF WELL	RECHARGE WELL		IG		1		Jan	even	Jul
WATER	2 STOCK 3 IRRIGATION	6 MUNICIPAL 7 PUBLIC SUPPL	Y		Å,	61			
USE	4 INDUSTRIAL	• [] COOLING OR A 9			3 (
METHOD	1 CABLE TOOL 2 ROTARY (CONVE	6 D B				T		• -	
OF CONSTRUCTIO	N A D ROTARY (REVER	ונ [] # (E) ום [] # ום []	ETTING RIVING Igging Dother	DRILLERS	REMARKS	•		25	232
NAME OF WELL CO	ONTRACTOR		WELL CONTRACTO		58 CE			0 4 404	····
ADDRESS	yht well	Jullers Fta	5507		OF INSPECTION		TED		
NAME OF WELL	TECHNICIAN	orth and	WELL TECHNIGIAN		PKS				0-
NO SIGNATURE OF T		SUBMISSION	7-0221			CSS.88			
Le lille	and he	DAY_	MO YR	ō			FOR	M NO. 0506	(11/86) FORM
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Ontario Env	rironment		VVA						.00	
COUNTY OR DISTRICT	2. CHECK 🗵 COR	TOWNSHIP BOROUGH. CIT	r. TOWN VILLA	GE T			10 BLOCK TRACT. SUR		<u> </u>	22 23 74
RRUCE		SAUGEEN						DATE COM	PLETED	54/8 #
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	10 12	, 11.3	301	25 26	625	30	L			47
GENERAL COLOUR			AND BED		ATERIA	GENERA			DEPTH	· FEET
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BROWN	SANO	GRAVEL							1.5'	19
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				-						
	<u></u>									
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				<u>_</u>						
						LLI L				
41 WAT		51 CASING & C		E RECOR			OF OPENING	31-33 DIAMET	ER 34-38 L	NGTH 39-40
AT - FEET		DIAM MATERIAL INCHES 12	THICKNESS	FROM .	10 13-16		AL AND TYPE	The	DEPTH TO TOP OF SCREEN	41-44 30
15-18	$ \begin{array}{c} $	8 ² GALVANIZED 3 CONCRETE 4 ³ OPEN HOLE	. 188 ,	. /	16	61	PLUGGIN	IG & SEAL	ING RECO	
20-23	FRESH 3 USULPHUR 4 MINERALS	17-18 19 17-18 19 2 GALVANIZED			20-23	DEPTH SE	TAT - FEET	MATERIAL AND	TYPE CEMEN	T GROUT KER. ETC)
25-28	$\begin{array}{c} \text{SALTY} 6 \Box \text{ GAS} \\ \hline \text{FRESH} 3 \Box \text{ SULPHUR} \\ 4 \Box \text{ MINERALS} \end{array}$	3 □ CONCRETE 4 □ OPEN HOLE 5 □ PLASTIC 24-25 26			27-30	10-13 O	3""	Семеля	GLOUT	-
30-33 I	FRESH 3 DSULPHUR 34 10 4 DMINERALS	1 STEEL 2 GALVANIZED 3 CONCRETE 4 OPEN HOLE				26-29	30-33 80			* 54
PUMPING TEST METI	SALTY 6 GAS	5 PLASTIC	MPING							
	2 G BAILER 25	3 GPNHOU	17-1 RS M15	ا		GRAM BELOV		ES OF WELL	ROM ROAD AN	D
LEVEL 19-21	END OF WATER L PUMPING 22-24 15 MINUTES	EVELS DURING 2 30 MINUTES 45 MINUTES	RECOVERY 60 MINUTES		LOT LI		CATE NORTH BY A	RROW		
	16 FEET FEE 38-41 DUMP INTAGE	29-31 32-3 ET FEET FEI WATER ALEND O	4 35-3 ET 16 FEI		15	<u>***</u>]	16	- 4	Z	
	GPM	FEET 1 DELEAR	* [] CLOUDY			ף ו				
C. RECOMMENDED PUM	IP TYPE RECOMMENDED PUMP DEEP SETTING	43-45 RECOMMENDED PUMPING FEET RATE	46-4 GP			R	BLOCK	<<		
	H				-#-					
FINAL STATUS	2 OBSERVATION WEL	S 🗌 ABANDONED, INSUFI L S 🗋 ABANDONED POOR 7 🗋 UNFINISHED	JUALITY	1 m						
OF WELL SS-	4 D RECHARGE WELL	DEWATERING	<u> </u>	385	25	71				
WATER	2 STOCK 3 IRRIGATION 4 INDUSTRIAL	D MUNICIPAL PUBLIC SUPPLY COOLING OF AIR CONDIT							7	1
		• 🗆 NOT	USED		1.7 S	4				
METHOD	CABLE TOOL	IONAL) 7 GATAMOND	below STE	••• ••-•			0	Qore	4	
CONSTRUCTIO	N 4 C ROTARY (AIR) A C AIR PERCUSSION		AUCEL YOTHER	DRILLEI	RS REMARKS	-		TOM	54	115
NAME OF WELL C		WELL	CONTRACTOR		A	58 CONI	TRACTOR 59-62	DATE RECEIVED	1.0	63-68 80
ADDRESS	CREAN URILL	ING LIMITED	129		E OF INSPECT		L C J	TAT		
A S-661	LOLDY DL WA	TERIOD DI-T. WELL LICEN	TECHNICIAN'S			·			T	
O MIK É SIGNATURE OF T	OLLICE TECHNICIAN/CONTRACTOR	SUBMISSION DATE	0268	FFIC	P),		('88 ei			
		DAY 30 NO.	04 yr.96	2 0				FOR	M NO. 0506 (11	/86) FORM 9

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Ontario Environ	MENT	CES PROVIDED		1407	481	4015		
COUNTY OR DISTRICT	2. CHECK 🛛 CORRECT	TOWNSHIP, BOROUGH, CITY,	TOWN. VILLAGE		CON	TO 14 BLOCK, TRACT, SURVEY	ETC	LOT 25-27
		<u> </u>		A			DATE COMPLETER	MO 01 VR 90
		23	<u>× 1840</u> 2 9.1 1 151	1 62 7	5			
	LOG	OF OVERBURDEN	AND BEDRO	CK MATER	IALS (SEE)	31 NSTRUCTIONS)		•
GENERAL COLOUR	MOST COMMON MATERIAL	OTHER MAT	ERIALS		GENER	AL DESCRIPTION		FROM TO
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GLEY			1310423				·.	
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		<u> </u>	- <u> </u>					
31								
				BECOBD		St OF OPENING	31-33 DIAMETER	34-38 LENGTH 39-4
WATER FOUND AT - FEET K	IND OF WATER	INSIDE DIAM MATERIAL	WALL THICKNESS FR	DEPTH - FEET		ERIAL AND TYPE	8	INCHES 3 FEE PTH TO TOP 41-44 SCREEN 41-44
8 ¹⁰⁻¹³ ¹ D FR ² SA	ESH 3 □ SULPHUR 14 LLTY 4 □ MINERALS 6 □ GAS	10-11 1 STEEL 1 2 GALVANIZED 3 GONGBETE		1	3.16 0 5	TAINERS ST	un l	16 FEET
15-18 1 _ FR 2 _ S/	RESH 3 USULPHUR 4 MINERALS ALTY 6 GAS	8 □ COPER HOLE 5 □ PLASTIC 17-18 1 □ STEEL	.188 +1	20	0-23 DEPTH		G & SEALIN	PE (CEMENT GROUT LEAD PACKER, ETC.)
20-23 1 [] FR 2 [] SA	RESH 3 SULPHUR 4 MINERALS 6 GAS 29	2 GALVANIZED 3 CONCRETE 4 OPEN HOLE 5 PLASTIC			0	10-13 S 14-17 C	emen 7	6 Row T
1 C FF 2 S/ 30-33 C -	ALTY 6 GAS	24-25 2 1	•	27	7-30 5	18-21 6.5 B 16-29 30-33 80	ENTONIT	e clay
2 3	ALTY 6 GAS	4 COPEN HOLE 5 DELASTIC		<u> </u>				
71 1 B FUMP 2		3 GPN 2 15	16 17-18 URS MINS	1	N DIAGRAM BE	LOCATION O	S OF WELL FR	OM ROAD AND
	ATER LEVEL END OF PUMPING 22-24 IS MINUTES	VELS DURING 2	RECOVERY	Ĺ	OT LINE II	NDICATE NORTH BY A	RROW.	2
	16 FEET FEE 38-41 PUMP INTAKE S	ZS-31 32 T FEET I ET AT WATER AT ENC	FEET 16 FEET		15	16		-
			R 2 CLOUDY			^k 16.₩'9.8		
SHALLOW		PUMPING FEET RATE	GPM					
EINAI 34	1. WATER SUPPLY	SABANDONED. INS	JFRICIENT SUPPLY	A 9)	BLOC	1 55	
STATUS OF WELL	2 OBSERVATION WEL 3 TEST HOLE 4 RECHARGE WELL	L S ABANDONED POO 7 UNFINISHED Dewatering	R QUALITY	δ δ				
55-54	1 DOMESTIC 2 STOCK	S COMMERCIAL						
USE	3 IBRIGATION 4 I INDUSTRIAL I OTHER	COOLING OR AIR CON D	DITIONING DT USED			4		
s7 METHOD	CABLE TOOL	6 🗋 BORING	Hollow		LOT 5	7		
OF	3 ROTARY (REVERSE 4 ROTARY (AIR) 5 ROTARY (AIR)) B _ JETTING 9 _ DRIVING	AnGth			HWY 21		54116
NAME OF WELL CO	NTRACTOR		LL CONTRACTOR'S		58	CONTRACTOR 59-62	DATE RECEIVED	63-64
ADDRESS	CLAIN PRILLI	NG LIMITED	1129		INSPECTION	IIZY INSPECTOR	<u> HAT </u>	0 1990
NAME OF WELL	TECHNICIAN	TELLOU WE	LL TECHNICIAN'S		, 01			-0
O MIKE SIGNATURE OF TE	CHNICIAN/CONTRACTOR	SUBMISSION DATE	<u>0268</u>		ΧĊ		S.Se	
MINISTRY O	F THE ENVIRON	MENT COPY) <u>~ 7</u> YR <u>/</u>	" L <u>'</u>			FORM	VI NO. 0506 (11/86) FOR

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of th	e						ELL	RE	CO	RD
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	1. PRINT ONLY IN 2. CHECK 🗵 CORR	SPACES PROVIDED	E 11	1	40//	<u> </u>	14015		kk	22 23 24
COUNTY OR DISTRICT		TOWNSHIP, BOROUGH.	CITY. TOWN, VILLA	GE		CON	BLOCK, TRACT, SURVEY	. ETC		Pt.51
			wp.					DATE COMP		41-53 ct
		<u>ک</u> ـ	I, Port El	gin, (NOH Z	CO BASIN CODE	DAY	<u>е мо</u>	
1 2		17	3256	25	2603	30	31			47
	LC		DEN AND BEI	DROCI	K MATERIAL	.S (SEE	NSTRUCTIONS		DEPTH	- FEET
GENERAL COLOUR	COMMON MATERIAL	OTHER	MATERIALS			GENER	AL DESCRIPTION		FROM	то
	Topsoil		·····						0	
Brown	Sand	Stones			Soft				1	21
Brown	Sand	Clay, stone	S ·		Hard				21	<u>21</u> 49
Grey	Clay	Stones			Solt				21 //9	91
Brown	Llay	Stones	·	•	Hard				91	131
Blue	Limestene	Stones			Mod	hard			131	197
	Limestone			<u>.</u>	Hard		<u> </u>		197	269
Dk.Diue	Limestone				Hard				269	305
Lt.Brown	Limestone				Med.	hard			305	384
Dubiowi										_
31										
32 1 2 10							54			
41 WA	TER RECORD	51 CASING	& OPEN HC				S) OF OPENING T NO)	31-33 DIAME	TER 34-38	LENGTH 39-40
WATER FOUND AT - FEET 10-13 1 73	KIND OF WATER	INSIDE DIAM MATERIA INCHES	WALL THICKNESS INCHES	FROM	то		ERIAL AND TYPE	I	DEPTH TO TOP OF SCREEN	41-44 30
384 2	SALTY 4 MINERALS 6 GAS	10-11 1 DISTEEL 2 DGALVANIZ 3 D CONCRETI	ED LOO		120					FEET
2] FRESH 3 USULPHUR 4 Ominerals 3 Salty 6 Gas	6 4 0 OPEN HOU 5 0 PLASTIC	.E .188	(20-23	61 DEPTH	PLUGGIN	G & SEAL	LING RECU	DRD
20-23 1 2] FRESH 3 □SULPHUR 24] A □ MINERALS] SALTY 6 □ GAS	1 DSTEEL 2 DGALVANIZ 3 DCONCRET	ED	132	-6 384	FROM	TO 0-13 14-17		LEAD P	ACKER. ETC)
25-28 1 2	FRESH 3 SULPHUR 29 SALTY 6 CALS	24-25 1 DISTEEL	26		27.30		8-21 22-25		·	
30-33 1	FRESH 3 DSULPHUR 34 B GALTY 6 MINERALS	0 2 GALVANIZ 3 GONCRET 4 OPEN HO	ED E LE			20	5-29 <u>30-33</u> 80			
PUMPING TEST ME	THOD 10 PUNPING RAT	E II-14 DURATION	1 OF PUMPING			<u>ــــــــــــــــــــــــــــــــــــ</u>			L	
		4 дрм _2	IS-16 HOURS	17-18 MINS		GRAM REI	OW SHOW DISTANCE	S OF WELL	FROM ROAD	
STATIC LEVEL	WATER LEVEL END OF PUMPING 22-24 IF MINIMUM	LEVELS DURING	PUMPING	TES	LOT LI	INE IN	DICATE NORTH BY A	RROW.	-	
Flowing		28 29-31 FET 69-FFT 9	32-34 37 FEET 101	35-37 FEET	1		,			4
Sive RATE	38-41 PUMP INTAKE	SET AT WATER A	T END OF TEST	42	$\langle - \cdot \rangle$	·	- Lot -	INE		r.
RECOMMENDED PU	GPM IMP TYPE RECOMMENDE PIIMP	130 FEET ' X ED 43-45 RECOMME PUMPING		16-49	L)		8'			
D. SHALLOW	W DEEP SETTING	130et RATE	4	GPM	A		WELL Ö	- 60	′ →	1
EINIA	54 1 SP WATER SUPPLY	S 🗋 ABANDONED.	INSUFFICIENT SUP	PLY	E		/ <u> / </u>			
STATUS	2 OBSERVATION WE	LL & ABANDONED 7 UNFINISHED	POOR QUALITY		/		/ #/		e	
	4 C RECHARGE WELL	DEWATERING		-	4 (~			0 A	
WATER	2 STOCK 3 IRRIGATION	6 D MUNICIPAL 7 D PUBLIC SUPPLY			$\frac{u}{k}$	PT.1	107 51		۵	
USE	4 🔲 INDUSTRIAL	COOLING OR AIR Society	CONDITIONING] NOT USED		o /					
METHOD	57 CABLE TOOL	* BOR	ING		~/					
OF	- L ROTARY (CONVEN 3 D ROTARY (REVERS ON 4 D ROTARY (AIR)	E) 4 01A1 DE) 4 0 JETT 9 0 DRIV	TING TING		{				8	5519
	S AIR PERCUSSION		SING OTHER		DRILLERS REMARK	<s< td=""><td></td><td></td><td></td><td></td></s<>				
NAME OF WELL	CONTRACTOR	Limited	WELL CONTRACT LICENCE NUMBE	R		58	1737	DATE RECEIVED	2 1 190	····آ
	N WEIT DETITING		<u> </u>		DATE OF INSPE	CTION	INSPECTOR			~ • - +
Box 48	16, Wingham, On	tario. NUG 2	WU WELL TECHNICI LICENCE NUMBI	AN'S ER			I		· Jr	
G. Wri	ght F TECHNICIAN/CONTRACTOR	SUBMISSION D	T0166		FFIC					
LOY	tanlon	<u>DAY 9</u>	MO NOV. YF	90.	ō			888 88 2		(11/86) 50014
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	ironment	WAT		ELL F	RECO	RD
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COUNTY OR DISTRICT		TOWNSHIP, BOROUGH, CITY, TOWN, VILLAGE	CON	BLOCK, TRACT, SURVEY E		LOT 25-27
		Archibald Place	- Southamaton O	shi (DATE COMPLETED	48-53 V 91.
		TOLE 74	E, Southampton, O	BASIN CODE	H IN	YR
<u> </u>						
GENERAL COLOUR	470 MOST	OTHER MATERIALS	665 GENER	AL DESCRIPTION	DEPTH	- FEET
-	Topsoil	· · · · · · · · · · · · · · · · · · ·			0	1
Brown	Sand	Gravel	Soft		1	6
Grey	Clay	Silt	Soft		6	17
Grey	Sand		Soft		17	32
Grey	Clay	Silt	Soft		32	44
·						
				· .		
41 WA	TER RECORD	51 CASING & OPEN HOLE	RECORD Z (SICE)	54 51 OF OPENING 31- 1 NO 1	33 DIAMETER 34-38	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
WATER FOUND AT - FEET	KIND OF WATER	INSIDE MATERIAL WALL DIAM MATERIAL THICKNESS INCHES F	DEPTH - FEET	18 slot	5.75 INCHES	3 FEET 41-44 30
17-32 ¹⁰⁻¹³	FRESH 3 SULPHUR SALTY 4 MINERALS 6 GAS	10-11 1 STEEL 12 2 GALVANIZED	13-16 00 St	ainless Steel	2	9 FEET
15-18 1 (2 (☐ FRESH 3 □SULPHUR ¹⁹] Salty 4 □Minerals] Salty 6 □Gas	6 4 DOPEN HOLE 5 PLASTIC -188 +	2 28 61		& SEALING RECO	DRD
20-23 1 [2 [☐ FRESH 3 □ SULPHUR ²⁴ ☐ SALTY 4 □ MINERALS 6 □ GAS	1 -18 1 STEEL 2 GALVANIZED 3 CONCRETE 4 GOPEN HOLE	20-23 FROM	TO MAT	ERIAL AND TYPE LEAD P	ACKER. ETC)
25-28 1 [2 [FRESH 3 USULPHUR 29 SALTY 4 MINERALS G GAS	24-25 1 DSTEEL 26	27-30 32	44 Sa	nd	
30-33 1 [2 [FRESH 3 SULPHUR 34 FRESH 4 OMINERALS SALTY 6 0 GAS	2 □ GALVANIZED 3 □ CONCRETE 4 □ OPEN HOLE 5 □ PLASTIC	26	-29 30-33 80		
71 PUMPING TEST ME	THOD 10 PUMPING RA	E 1-14 DURATION OF PUMPING		OCATION OF	WELL	
STATIC	2 DAILER	20 GPM HOURS MINS HEVELS DURING 1 C PUMPING	IN DIAGRAM BEL	OW SHOW DISTANCES C	OF WELL FROM ROAD	ND
LEVEL 19-21	PUMPING 1 22-24 15 MINUTES 26	2 XRECOVERY . 30 MINUTES 45 MINUTES 60 MINUTES 28 29-31 32-34 35-37	0.40km	South To	(2	シー
S IF FLOWING	T 11 FEET 9 F	EEET 8 FEET 8 FEET 8 FEET 8 FEET 12 FEET 13 FEET 14	Lor	LINE		
		26 FEET 1 CLEAR 2 CLOUDY	SAUGEEN	(ON. 10)	ROAD	
	W DEEP SETTING	20 FEET RATE 10 GPM				
50-53	54				·	
FINAL STATUS	2 DOBSERVATION WE	CLL 6 ABANDONED POOR QUALITY 7 UNFINISHED		500		· iu
	A D RECHARGE WELL	D DEWATERING COMMERCIAL				2
WATER	2 STOCK 3 IRRIGATION	MUNICIPAL PUBLIC SUPPLY GOOLING OD ND CONDITIONING		WELL	+ 250 ->	75
USE					fifi	2
METHOD	57 I CABLE TOOL 2 ROTARY (CONVE)	6 DORING NTIONAL) 7 DIAMOND	Lota	Lavek	PAUCE	Pak
CONSTRUCT	3 C ROTARY (REVERS 4 ROTARY (AIR) 5 AIR PERCUSSION	E) 1 DISTING 9 DRIVING DISGING OTHER		LAKEN	099	9603
NAME OF WELL	CONTRACTOR	WELL CONTRACTOR'S		CONTRACTOR 59-62 DAT	**************************************	9 63-68 10
Davidse	on Well Drilling	Limited 1737	DATE OF INSPECTION	1737		
NAME OF WE	Wingham, Ontar	Ivell technician's				X
C. Rea	TECHNICIA CONTRACTOR	SUBMISSION DATE	FICE			
1219	Donel	DAY 23 No. May YR 9	. ⁵	CSS.58		
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			<u>, /5</u> 0	<u>x 1840 1</u>	ORT ELL			
	NA		OF OVERBURDEN	AND BEDROCH	Z6 (MATERIAL	30 31 S (SEE INSTRUCTI	IONS)	
GENERAL	COLOUR	MOST COMMON MATERIAL	OTHER MAT	ERIALS		GENERAL DESCR	NPTION	FROM TO
			A					
		WELL 4	IAS PULL	ED 047	WIT	74 BA	CKHOE	
		HOLE WA	S BACKF	TLLED	WITH	NATIUR	SAND	
		9 BEN	SEAL MIX	· TO :	SURFAC	E		
31								
$\begin{bmatrix} 32 \\ 1 \\ 2 \end{bmatrix}$			51 CASING &			SIZE (S) OF OPEN	NING 31-33 DI	AMETER 34-38 LENGTH 39-40
WATER F AT - F			INSIDE DIAM MATERIAL INCHES	WALL DE THICKNESS INCHES FRUN	PTH · FEET	MATERIAL AND) TYPE	INCHES FEET DEPTH TO TOP 41-44 30 OF SCREEN
	10-13 1 1 1 2 1 1 15-18 1 0	FRESH 3 DSULPHUR SALTY 4 DMINERALS 6 DGAS 19 19	10-11 1 □ STEEL 2 □ GALVANIZED 3 □ CONCRETE 4 □ CONCRETE	2	13-16		ULIGGING & SE	
	20-23 1	A DININERALS SALTY 6 DGAS		9	20-23	DEPTH SET AT -	FEET MATERIAL	AND TYPE (CEMENT GROUT LEAD PACKER ETC.)
	2 25-28 1	SALTY $\begin{array}{c} 4 \\ \Box \\ 6 \\ \Box \\ GAS \end{array}$ FRESH $\begin{array}{c} 3 \\ \Box \\ SULPHUR \\ 4 \\ \Box \\ MINERALS \end{array}$	3 CONCRETE 4 OPEN HOLE 5 DPLASTIC 24-25	6	27-30	190-13	0 BACK	FILLED WINATION
	30-33 1 [] 2 []	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2 □ GALVANIZED 3 □ CONCRETE 4 □ OPEN HOLE 5 □ PLASTIC			26-29	30-33 80	+ ISRNSFAL
71	APING TEST METHO	DD 10 PUMPING RATE	11-14 DURATION OF I	PUMPING -16 17-18		LOCA	TION OF WI	ELL
	STATIC LEVEL	WATER LEVEL 25 END OF WATER LE PUMPING	GPMHO 1 [] VELS DURING 2 []	PUMPING RECOVERY	IN DIA Lot L	GRAM BELOW SHO	W DISTANCES OF WE	LL FROM ROAD AND
TES1	19-21 FEET	22-24 15 MINUTES 24-20 FEET FEET	30 MINUTES 45 MINUTES 29-31 31 FEET	S 60 MINUTES 2-34 35-37 FEET FEET		15	1	6 77
MPIN	FLOWING. VE RATE	GPM	FEET 1 CLEA	R 2 CLOUDY	Λ	9.8 1		
D .	COMMENDED PUMP	TYPE RECOMMENDED PUMP DEEP SETTING	43-45 RECOMMENDED PUMPING FEET RATE	GPM	mar 1	49.	2' BLOCK	55
	FINAL	4 WATER SUPPLY	S ABANDONED INSI	UFFICIENT SUPPLY) M			
	STATUS OF WELL	2 DESERVATION WELL 3 TEST HOLE 4 RECHARGE WELL	7 DUNFINISHED	GUALITY	385			
	water	S6 I DOMESTIC 2 STOCK 3 IRRIGATION	5 COMMERCIAL 6 MUNICIPAL 7 PUBLIC SUPPLY					
	USE	A D INDUSTRIAL	COOLING OR AIR CON D N	DITIONING OT USED	Lo	5 54		
N	AETHOD OF	 CABLE TOOL CABLE TOOL ROTARY (CONVENT ROTARY (REVERSE 	6 🗌 BORING IONAL) 7 🗍 DIAMON 9 🔒 🗍 JETTING	D			Hwy 2	54229
CON	STRUCTIO	N 4 C ROTARY (AIR) 5 AIR PERCUSSION		G OTHER	DRILLERS REMAR	RKS		J4223
R	AME OF WELL C	CONTRACTOR	NG LIMITED	LL CONTRACTOR'S ENCE NUMBER			OR 29 DATE REC	JAN 1 6 2003
RACTC	100RESS	COLOY DE L	NATERION ONT	NAVICZ				
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of the Envir	e ronment	WA	EER	WELL	RECO	ORD
Ontario	1. PRINT ONLY IN S 2. CHECK 🛛 CORRE	PACES PROVIDED ABA	NDONM	RIGINAL HOL	5 La # 5	
COUNTY OR DISTRICT	E	TOWNSHIP, BOROUGH, CITY, TOWN, VILLAGE		CON . BLOCK, TRACT. SU		55
		3,× 1840	lort KIGIN	DAT.	DAY 13 NO 1	1/ _{YR} 02
21						
	LO Most	G OF OVERBURDEN AND BED	ROCK MATERIA	LS (SEE INSTRUCTIONS) GENERAL DESCRIPTION	DE FROM	PTH - FEET
GENERAL COLOUR	COMMON MATERIAL					
	WELL WA	S PULLED OUT	WITH	BACKHOE		
	HOLE WAS	BACKFILLED W	NAT NAT	JUE SAND	9	
	BENSEAL	MIX TO	SURFACE	•		
31	<u> </u>					
					31-33 DIAMETER 34	-38 LENGTH 39-40
41 WA		51 CASING & OPEN HO	DEPTH - FEET			HES FEE
10-13 1 (2 (☐ FRESH 3 □ SULPHUR 14 □ SALTY 4 □ MINERALS 6 □ GAS		FROM TO 13-16	S S	OF SCREE	N FEET
15-18 1 2	□ FRESH 3 □ SULPHUR □ FRESH 4 □ MINERALS □ SALTY 6 □ GAS		20.21	61 PLUGO	SING & SEALING R	
20-23 1 2	FRESH 3 SULPHUR 4 MINERALS 5ALTY 6 GAS	1 □ STEEL 2 □ GALVANIZED 3 □ CONCRETE 4 □ OPEN HOLE		FROM TO 10-13 14-17	ACV CILLED	LAD PACKER ETC 1
25-28 1	□ FRESH 3 □ SULPHUR 4 □ MINERALS □ SALTY 6 □ GAS	5 □ PLASTIC 24-25 1 □ STEEL 2 □ GALVANIZED	27-30	18-21 22-25	SAND & BE	NSEAL
30-33 1 2	☐ FRESH 3 □ SULPHUR 34 4 □ MINERALS □ SALTY 6 □ GAS	A CONCRETE A COPEN HOLE 5 DPLASTIC		26-29 30-33	80	
71 PUMPING TEST N. 1 D PUMP	ETHOD 10 PUMPING RAT 2 D BAILER	E 11-14 DURATION OF PUMPING 15-16 1 GPMHOURS N	7-18 (INS			
STATIC LEVEL	WATER LEVEL END OF PUNPING 1 22-24 15 MINUTES			LINE INDICATE NORTH	BY ARROW.	27
S 1 5 5	ET FEET F	28 29-31 32-34 3 EET FEET FEET	5-37 FEET		14	V
GIVE RATE	38-41 PUMP INTAKI GPM	FEET 1 CLEAR 2 CLOL		/3	<u>16</u> [9.8'	
C RECOMMENDED F	PUMP TYPE RECOMMEND PUMP DW DEEP SETTING	ED 43-45 RECOMMENDED 4 PUMPING FEET RATE			6.4 [′] O	
50-53	54 1 (1) WATER SUPPLY	S 🗋 ABANDONED. INSUFFICIENT SUPF	88			
STATUS	2 OBSERVATION W 3 TEST HOLE	ELL 6 ABANDONED POOR QUALITY 7 UNFINISHED			. 1 55	
	55-56 1 DOMESTIC	S COMMERCIAL		Brok		
WATER USE	3 DIRRIGATION 4 DINDUSTRIAL	7 DUBLIC SUPPLY 0 COOLING OR AIR CONDITIONING 9 NOT USED				
	57 1 CABLE TOOL	• BORING		bt 54		<u></u>
CONSTRUCT	2 ROTARY (CONVE 3 ROTARY (REVER 4 ROTARY (AIR) 5 AIR PERCUSSION	NTIONAL) / L DIAMOND SE) # C JETTING 9 C DRIVING 1 DIGGING OTHER	- DRILLERS REM	ARKS	HWY XI	54227
NAME OF WEL	RAIN PRILLING	LIMITED 1129	OR'S R N ODATE OF INS	SE CONTRACTOR 112 SPECTION HISPEC	59-62 DATE RECEIVED	1 6 2003
3-661	COLDY PR. WA	TELLOO OUT NUN ICZ				
	TECHNICIAN/CONTRACTOR	SUBMISSION DATE	OFFIC		U)3 .E.33
	Y OF THE ENVIRON				FORM NO.	0506 (11/86) FORM

(()	Ontario	Ministry of the Environment	Well Tag No. for N	laster We	ell (Place	e Sticker and/or Print Below) Master Well Record for
			A 05467	7	Д	Cluster Well Construction
Master W	lell Owner's and	Land Owner's Inform	mation			age/ of
First Name	- 11 car	Last	Name 2			E-mail Address
Aailing Add	Iress (Street Numbe	<i>4.66 (12001</i> pr/Name, RR)	Municipality			Province Postal Code Telephone No. (inc. area code)
<u>678</u>	33 WELLT	UG TON Rd. 3	4 Cambr	rfogi		ONT. NI3121014 5119 16151816161516
ddress of	and Construction	on of the Master Wel	l in the Cluster	shin		
	.		5	DUGE	En	40,49,50 / ALF RADIAE
ounty/Dis	trict/Municipality	<u>(</u>	City/1	Town/Villag	je	Province Postal Code
TTM Coordi	nates Zone Easti	ing Northing	GPS Ur	<u>⊭⊘⊁_S/</u> nit Make	(<i>U (1È É</i> Model	EN ShOLE> Unitario I Mode of Operation: Undifferentiated
NAD	8311746	7788 492	2025			Differentiated, specify
Overbu General	Irden and Bedroc Most Common	k Materials (see instru Other	ictions on the back General	of this fo	orm) (Metres)	Hole Details
Colour	Material	Materials	Description	From	To	From To Diameter (Centimetres)
rown	Sitt			0	6.5	504.615
land	SOND	crovel		0.5	119	
Goul	50010	5.4		1,9	4.6	
			······································		12	
		· · · · · · · · · · · · · · · · · · ·				Water Use
	·····		17.417 -11.1 .1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1			Domestic Commercial Dewatering
	······			E		
			······			Method of Construction
	· · · · · · · · · · · · · · · · · · ·					Cable Tool Air Percussion Digging
				1		Rotary (Reverse) Detting Other, specify
			· · · · · · · · · · · · · · · · · · ·	••••		
	P24491A1A1A1AAAA		·······	1		Status of Well
				<u> </u>		Replacement Well Abandoned, Poor Water Quality
					 	Dewatering Well Other, specify Alteration (Construction) Abandoned, other, specify
						No Casing and Screen Head Static Mater Loval Tech
1					• • •	Open Hole
side Diam	eter	Construction Deta	ils Wall	Deoth (Metresi	
Centimetre	es) (steel, plastic,	fibreglass, concrete, gal	vanized) Thickness	From	To	Galvanized Steel Fibreglass Concrete Plastic
1.9	PL0	Stic	0.4	0	4,6	2 Outside Diameter (Centimetres) Slot No. 2 2.7
						Water Details
						Water found at Depth Kind of Water
						Water found at Depth Kind of Water
	Annular	Space/Abandonment	Sealing Record	1		Metres Gas Fresh Salty Sulphur Minerals
pth Set at From I	(Metres) To	Type of Sealant Use (Material and Type)	ed	Volume (Cubic I	Used Metres)	Water found at Depth Kind of Water
0	1.6 13	ento uto				Disinfected Tyes TNo If no provide reason: Date Master Well Completed
.6 4	1.6 5M	10				(yyyy/mm/dd)
						Cluster Information (Please also fill out the additional Cluster Well
						Information for Well Construction for each parcel of land and cluster.) Total Wells in Cluster Please indicate Number of Cluster Well
		·····				Information Log Sheets Submitted
						- 1 I otal Wells on this Property 2
	2					Location of Well Cluster
						Detailed Map must be provided as an attachment no larger than legal size (8.5" x 14"). Sketches are not allowed.
						Check box to confirm detailed map is provided as per Section 11.1 (3)
		·····				Consent to release additional information concerning the cluster to the Director upon request
						Signature of Technician/Contractor Date (yyyy/mm/dd)
iness Nam	Well Contractor	actor and Well Techn	ician Information	actorie Lie-		Master Well Owner's/Land Owner's consect to 2007/10/03
			weil Contr			Cluster Form





Well Tag No. for Master Well (Print Well Tag No.)

A054677

Cluster Well Information for Cluster Well Construction

Regulation 903 Ontario Water Resources Act

	H()5	9677		Page of	f <u>3</u>
Property Owner's Information				C	
First Name Last Name	Mailing Address (Street No.	/Name, RR) Municipality		Pr	
REIDS HERITAGE GROUP	6783 WELLEN	GTON Rd 34 CAMBRIE	1 <u>6</u> E	Sig	
\mathcal{OM}_{1} $\mathcal{N}_{3} \subset \mathcal{I} \mathcal{V} \mathcal{I}$	Address	S / 9 6	86656		
Cluster Well Information				Co	
Address of Well Location (Street Number/Name, RR)	16,47 Concession Township	County/District/Mu	nicipality	upon request Signature of Technician/Contractor	Date (unu/mm/dd)
City/Town/Village Province Postal Code	GPS Unit Make Model	Init Mode of Operation			1. alestas
TOWN of SAUGEONS LODIES Ontario		Differentiated, specify:			2001/1903
Well # UTM Coordinates Full Depth of Hole Diameter on Sketch Zone Easting Northing Hole (metres) (cm)	Method of Casing Material Casing Length Construction (metres)	Screen Interval (metres) Annular Space Static Water From I To Sealant Used Level (metres)	Abandonment Sealant Used	Comments	Date of Completion
201 17 46 8 3 4 9 49 2 3 3 3 9 4.6 13.	Boring PLOSE 2.2	4.6 116 Bentinite 2.0	-		
203174681174922964 1.6 15	Baring PLASTIC 1.2	1.6 O.b Bestante 0.10			- Lang
204 1746799249228604.615	BORENH PLASHIC 2.2	4.6 1.6 Bertavite 0.6			102
205 1 7 4 6 7 8 7 4 9 22636 2.1 15	Boring Prostic 1.5	2.3 0.9 Benfante 0.3			BEC
206174678334922470 5.0 13	Baring Prostic 3.8	3.2 Bertonite 0.4			
207 17 46 7771491222735.0 15	Buring PLASTic 3.8	3.2 Bestavite 1.3			
2081746789249219904,615	Moring PLASTIC 3.4 1	7.6 3.8 Bertonike O16			
210 1746798949220611416 3	Boring PLOSTic 3.4	7.4 2.8 Bentowite 6.6			
211 17468093492201924615	Moring PLOSTIC 3.4	7.6 2.8 Berlante 0.6			
2121746781059992221414.6 15,	Boring Prostic 2.1 :	3. D I.S Benfarite 0.2			
Well Contractor and Well Technician Information Business Name of Well Contractor	ness Address (Street Number/Name, RR)	Municipality	Province	Date 1st Well in Cluster Constructed Date Last Well in (yyyy/mm/dd) 2007/10/02 (yyyy/mm/dd) 2007/10	Cluster Constructed
GEO-ENERMINTOL Millin 340	O MARLER Pr.	LARE TRAI	DIT	Ministry Use Only	
Postal Code $L = T \leq A = 4$ Business Telephone No. (inc. area code) $L = T \leq A = 4$ Business Telephone No. (inc. area code) T = B = 7 = 6 Business Telephone No. (inc. area code) T = 7 = 7 = 7 = 7 Business Telephone No. (inc. area code) T = 7 = 7 = 7 = 7 = 7 = 7 = 7 =	Well Contractor's Licence No. Business E-mail Ac $6 6 0 7$	Idress		Date Received (yyyy/mm/dd) Date Inspected	l (yyyy/mm/dd)
Name of Well Technician (First Name, Last Name)	Well Technician's Licence No. Date Submitted (yy)	y/mm/dd) Signature of Technician		Audit No. 00712 Remarks	
1991 (11/2008)	3 1 0 7 200 10	X.		C UUIIS MOOG	
1991 (11/2000)		lstry's Copy		© Queen's Printe	er for Ontario, 2006





Ministry of the Environment

Well Tag No. for Master Well (Print Well Tag No.)

Prop	erty Owner'	s Information					*							Consent
First I	lame	Last	Name		~~~~~ <u>~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~</u>	Mailing Add	Iress (Street N	o./Name, F	RR)	Munici	pality		<u> </u>	Property Owner's Consent to
Provir	<u>ZEIRS</u>	<u> 1-68/2573/52</u> (5 Postal Co	<u>, 2008</u> de	 E-mai	Address	6783	3 Crocci	The Ton	<u>rd</u>	34 COM	h <u>Beto</u>	<u>(74</u>		
	GIT.	113	621	14						5 7 9	716 E	6665	6	
Clus	ter Well Info	rmation	i				······							Consent to release additional
Addre	ss of Well Locati	on (Street Number/Name, RF	R)	Lot	46,417 C	Concession 7	Fownship			County	y/District/Mui	nicipality		upon request
City/Te	wn/Village	Provi	ince Po	Stal Code	<u>, 49,58 (1</u>	<i>OLLE PANULU</i> GPS Unit Make IN	<u>>50G60</u> Model	ビル Unit Mod	le of Oper	ation TUn	ruce Hifferentiated			
low	~ of SSC	GEENSGORES Ont	ario					Differe	entiated, s	pecify:			«	
Well # on Sketch	U Zone Easting	TM Coordinates Northing	Full Depth of Hole (metres)	Hole Diameter (cm)	Method of Construction	Casing Material	Casing Length (metres)	Screen Inte	erval (metres)	Annular Space Sealant Used	Static Water Level (metres)	Abandonment Sealant Used		Comments
214	17467	9884922227	4.6	15	Baring	PLOSTic	3,4	4.6	2.3	Benderike	0.5	<u></u>		
215	17468	1114922173	4.6	15	Buring	PLOSTic	3,4	4.6	2.8	Bestante	6,5			
217	17468	1414922026	4,6	13	Boring	PLOSTic	2.1	3.0	15	Bertowike	0,3			
														······
					·····						·····			
														·····
».														
Well	Contractor a	nd Well Technician In Contractor	formation	Busi	noss Addross ()	Stroot Number/Ma			Musician	14				Date 1st Well in Cluster Constructed
61	G-CNUL	AMUNTAL Mr.	lin		40 MADI	Chrd Dw				A Trace		Province		Ministry Ilse Only
Postal	Code FTIZIA	Business Telephone N F/ G/12 G 7	10. (inc. area (7 6 2	code) 3 9 1 9	Well Contractor	r's Licence No. Bus	siness E-mail A	ddress	<u> </u>	c100				Date Received (yyyy/mm/dd)
Name	y Well Technicia	n (First Name, Last Name)			Well Technician	n's Licence No. Dat	e Submitted (y)	/yy/mm/dd)	Signature	of Technician		,		Audit No.
	y GAMI	in			31	09			4			≈ * *		ç UU/12
1991 (11	7/2006)						291	histry's (Copy					

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Cluster Well Information for Cluster Well Construction

A054677



APPENDIX B

BOREHOLE LOGS

	CR	ING INC	CMT Engineering Inc. 1011 Industrial Crescent, St. Clements, ON, N0B 2M0 Telephone: 519-699-5775	PROJECT: _M	iramichi	Shor	res - Pha	SOREHOLE NU	JMBER B	H20-01 GE 1 OF 1
				PROJECT ADD	RESS:					
PRO	JECT N	UMBER: _20)-626	PROJECT LOC	ATION:	Sau	ugeen Sl	hores, Ontario		
DRIL	LING D	ATE: 20-11	-16	GROUND ELE	ATION:	18	4.60 m			
DRIL		ONTRACTOR	R: <u>CMT Drilling Inc.</u>	LOGGED BY:	SW	0.07	-			
DRIL			Geoprobe 7822D1	SAMPLING ME	THOD:	SPI				
DEPTH (m)	GRAPHIC LOG	٨	IATERIAL DESCRIPTION	Depth, Elevation (m)	SAMPLE TYPE NUMBER	RECOVERY %	BLOW COUNTS (N VALUE)	▲ SPT N VALUE ▲ 10 20 30 40 ⊗ POCKET PEN. (kPa) ⊗ 90 180 270 360 ● MOISTURE CONTENT (%) ● 12 24 36 48	WELL DIA	AGRAM
	~~	TOPSOI	L Very loose, black, sandy	0.00, 184.60						
		DISTUR brown re and clay	BED SAND Very loose, dark eworked/disturbed sand, trace silt , some organics, moist	0.13, 184.47	SPT 1	20	0-1-1-1 (2)	2 19.9●	Ber	ntonite al
1		SAND Locay, sat	oose, brown sand, trace silt and urated	0.76, 183.84	SPT 2	44	1-2-2-2 (4)	4	Wa 183 Dec	ter Level: .877 m on : 8/2020
2		Becomir	ng grey, compact	1.52, 183.08	SPT 3	100	4-6-5-5 (11)	24.8		
20-05-15.01 21-01-18 0					SPT 4	100	4-7-9 (16)	22.8		
		Compac (Based o by SPT	rt, saturated sand, trace clay and silt on visual inspection. Not confirmed sampling)	t 3.05, 181.55					-#3 S	Sand Pack mm een
≤ H	-[:•:•:									
N	-	Rottor	m of borehole at 4 57 m. Elevation							
BOREHOLE		2010	180.03 m.							

		CI	ING INC	CMT Engineering Inc. 1011 Industrial Crescent, St. Clements, ON, N0B 2M0				B	SOREHOLE NU	IMBER	BH20-02 PAGE 1 OF 1
	ENC	INEEK		Telephone: 519-699-5775	PROJECT: M	iramichi	Shor	res - Pha	ase 4 Subdivision		
					PROJECT ADD	RESS:					
	PROJ	ECT N	UMBER: _20)-626	PROJECT LOC						
	DRILL	ING D	ATE: 20-11	-16	GROUND ELEV	/ATION:	_18	4.91 m			
		ING C	ONTRACTOR	R: <u>CMT Drilling Inc.</u>	LOGGED BY:	SW	0.07	-			
	DRILL			Geoprobe 7822D1	SAMPLING ME					1	
	DEPTH (m)	GRAPHIC LOG	Ν	IATERIAL DESCRIPTION	Depth, Elevation (m)	SAMPLE TYPE NUMBER	RECOVERY %	BLOW COUNTS (N VALUE)	▲ SPT N VALUE ▲ 10 20 30 40 ⊗ POCKET PEN. (kPa) ⊗ 90 180 270 360 ● MOISTURE CONTENT (%) ●	WELL	DIAGRAM
$\left \right $		$\sim \sim$	TOPSOI	L Very loose, black, sandy	_0.00, 184.91			_	<u>12 24 36 48</u> <u>:</u> : : :		
	-		topsoil, DISTUR reworke trace org Becomin	moist (80 mm) BED SAND Very loose, grey d/disturbed sand, trace silt and clay, ganics and roots, moist (200 mm) ng red	0.08, 184.83	SPT 1	66	0-1-1-1 (2)			Bentonite Seal
			SAND L	oose, grey sand, trace silt and t	1.04, 183.87	SPT 2	70	3-4-5-4 (9)	23.1		38 mm Riser
	- - -		Becomir	 ng saturated	1.52, 183.39	SPT	61	4-4-4-4	8		Vater Level: 183.645 on Dec 8/2020
	2					3		(8)	23.7		
01-10-17 100-01-00-0	- - - 3		Becomin	ig compact	2.29, 102.02	SPT 4	100	5-5-6 (11)	22.8		
	-		Compac (Based by SPT	et, saturated sand, trace clay and silt on visual inspection. Not confirmed sampling)	3.05, 181.86						t3 Sand Pack
											38 mm Screen
	-										
			Bottor	n of borehole at 4.57 m, Elevation 180.34 m.							

		CI	MANC	CMT Engineering Inc. 1011 Industrial Crescent, St. Clomonto, ON, NOB 2000				E	SOREHOLE NU	JMBER	BH20-03 PAGE 1 OF 1
	NGI	NEER		Telephone: 519-699-5775	PROJECT: M	iramichi	Shoi	res - Pha	ase 4 Subdivision		
					PROJECT ADD	RESS:					
PR	OJE	CTN	UMBER: _2	0-626	PROJECT LOC	ATION:	Sau	ugeen Sl	hores, Ontario		
DR	ILLI	NG D	ATE: 20-1	1-16	GROUND ELEV	ATION:	18	2.90 m			
DR	ILLI		ONTRACTO	R: <u>CMT Drilling Inc.</u>	LOGGED BY:	SW					
DR		NG E	QUIPMENT:	Geoprobe 7822D1	SAMPLING ME	THOD:	SP			1	
DEPTH	(m)	GRAPHIC LOG	ſ	MATERIAL DESCRIPTION	Depth, Elevation (m)	AMPLE TYPE NUMBER	ECOVERY %	-OW COUNTS (N VALUE)	▲ SPT N VALUE ▲ 10 20 30 40 ⊗ POCKET PEN. (kPa) ⊗ 90 180 270 360 ● MOISTURE CONTENT (%) ●	WELL	DIAGRAM
						S	Ľ.	B	12 24 36 48		
			TOPSO topsoil, DISTUR reworke some o SAND v silt and	IL Very loose, black, sandy moist (100 mm) IBED SAND Very loose, brown ed/disturbed sand, trace silt and cla rganics, moist (100 mm) /ery loose, light brown sand, trace clay, moist	0.00, 182.90 0.10, 182.80 0.20, 182.70 y	SPT 1	61	0-1-1-1 (2) 5	2		Bentonite Seal
			Becomi	ng loose, grey, wet	0.76, 182.14	SPT 2	20	3-2-3-3 (5)	.5		88 mm Riser
						SPT 3	61	2-2-5-5 (7)	23.4		Vater Level: 81.38 on Dec 8/2020
81-10-12 100.01-c0			Becomi	ng compact, saturated	2.29, 180.61	SPT 4	100	2-6-9-9 (15)	15 24.8		
			Compad (Based by SPT	ct, saturated sand, trace clay and s on visual inspection. Not confirmed sampling)	ilt 3.05, 179.85 1						∜3 Sand Pack
	 										88 mm Screen
> H	-										
			Botto	m of borehole at 4.57 m, Elevation 178.33 m.				<u> </u>			

	GR	MGINC	CMT Engineering Inc. 1011 Industrial Crescent, St. Clements. ON. N0B 2M0				В	OR	EHO	LE	NL	JMBER	BH20-04 PAGE 1 OF 1
ENC	INEER		Telephone: 519-699-5775	PROJECT: <u>M</u>	iramichi RESS:	Shor	es - Pha	se 4 Si	ubdivisi	on			
PROJ		UMBER: _20)-626	PROJECT LOC									
DRILL	ING D	ATE: 20-11	-16	GROUND ELEVATION: 180.78 m									
DRILL	ING C	ONTRACTOR	R: CMT Drilling Inc.	LOGGED BY: _SW									
DRILL	ING E	QUIPMENT:	Geoprobe 7822DT	SAMPLING ME	THOD:	SP	Γ						
DEPTH (m)	GRAPHIC LOG	Ν	Depth, Elevation (m)	SAMPLE TYPE NUMBER	RECOVERY %	BLOW COUNTS (N VALUE)	▲ SPT N VALUE 10 20 30 ⊗ POCKET PEN. (kF 90 180 270 ● MOISTURE CONTEN 10 01 07			40 a) ⊗ 660 - (%) ● 48	- WELL	DIAGRAM	
-	$\sim \sim$	TOPSOI topsoil.	L Very loose, black, sandy wet (220 mm)	0.00, 180.78						:	:		
-		DISTUR reworke and clay saturate	BED SAND Very loose, grey d/disturbed sand, trace gravel, silt <i>r</i> , some organics, trace wood, d	0.22, 180.56	SPT 1	0	0-0-1-1 (1)			•	>>		Water Level: 180.425 m on Dec 8/2020
-		BURIED	TOPSOIL Very loose black silty	0.86 179.92									38 mm Riser
1		organic (100mm DISTUR reworke and clay	burried topsoil layer, saturated BED SAND Very loose, grey d/disturbed sand, trace gravel, silt v, trace organics, trace wood, d	0.96, 179.82	SPT 2	100	0-1-0-1 (1)			55	5.4		Bentonite Seal
					SPT 3	80	0-0-2-2 (2)	2	39	.3•	· · · · · · · · · · · · · · · · · · ·		#3 Sand Pack
20-05-15.GDI 21-01-18 		SAND C silt, clay	compact to dense, grey sand, trace and gravel, saturated	2.29, 178.49	SPT 4	100	4-9-17-20 (26)	21	.8		· · · · · · · · · · · · · · · · · · ·		38 mm Screen
JOREHOLE LOG WITH WELLZ ZU-526 - BH LUGS GFU UMI_IEMTLATE_		Bottor	n of borehole at 3.05 m, Elevation 177.73 m.										

TABLE B-1(A): MONITOR CONSTRUCTION DETAILS

Miramichi Shores Phase 4 PTTW Report (Project 20007.00)

	MONITOR CONSTRUCTION DETAILS											
Monitor	Depth (mbgl)	BH Dia. (mm)	Monitor Dia. (mm)	Screen Length (m)	Sand Pack	Casing Elev. (masl)	casing stickup (magl)	ground Elev. (masl)	Creek Bed Elev (masl)			
BH20-01	4.57	200	38	1.52	#3	185.62	1.03	184.59				
BH20-02	4.57	200	38	1.52	#3	185.95	0.97	184.98				
BH20-03	4.57	200	38	1.52	#3	183.97	1.03	182.94				
BH20-04	3.05	200	38	1.52	#3	181.82	0.98	180.84				
DP20-01	2.36*	38	38	0.9	na	181.44	1.24*		180.20			

Note: monitor depth and casing stickup for DP20-01 are relative to creek bed

TABLE B-1(B): WATER LEVELS

	Groundwater and Surface Water Levels												
	BH20	0-01	BH2	20-02	BH2	0-03	BH2	0-04	DP20-01	Creek			
Date	Water	Level	Water Level		Wate	r Level	Water	Level	Water Level				
	(mbtoc)	(masl)	(mbtoc)	(masl)	(mbtoc)	(masl)	(mbtoc)	(masl)	(masl)	(masl)			
16-Nov-20	1.780	183.840	2.260	183.690	2.580	181.390	1.390	184.230	na	na			
27-Nov-20	1.750	183.870	2.305	183.645	2.596	181.374	1.388	180.432	na	na			
8-Dec-20	1.743	183.877	2.305	183.645	2.585	181.385	1.395	180.425	na	na			
23-Dec-20	1.740	183.880	2.300	183.65	2.590	181.380	1.390	180.430	180.33	180.44			

APPENDIX C

HYDRAULIC CONDUCTIVITY TESTS
























APPENDIX D

DEWATERING CALCUATIONS

Table D-1: Construction Dewatering Unconfined Conditions K(avg) & 100 m Trench

Miramichi Shores Phase 4 Hydrogeological Report PTTW (Project 20007.00) (Method: Powers, 1992)



Table D-2: Construction Dewatering Unconfined Conditions K(max) & 100 m Trench

Miramichi Shores Phase 4 Hydrogeological Report PTTW (Project 20007.00) (Method: Powers, 1992)



Table D-3: Construction Dewatering Unconfined Conditions- Sensitivity Anlysis

Miramichi Shores Phase 4 Hydrogeological Report PTTW (Project 20007.00) (Method: Powers, 1992)



TABLE D-4 SUMMARY OF LAKESIDE WOODS DEWATERING (2018)

Project: Miramichi Bay Shores Phase 4 Hydrogeological Report Permit To Take Water (20007.00)

	PUMP 1						PUMP 2					TOTALS		
Date	Time	Meter Reading	Litres	hours	L/min	L/day	Time	Meter Reading	Litres	hours	L/min	L/day	L/min	Litres/day
Aug. 2	8:30 AM	22,313,100	0	0	0.0	0								
Aug. 3	8:30 AM	22,359,193	46,093	24	32.0	46,093								
Aug. 7	8:30 AM	22,368,469	9,276	96	1.6	2,319	3:00 PM	81,154,050	0	0	-	0		
Aug. 8	12 Noon	22,398,489	30,020	27.5	18.2	26,199	12:30 PM	81,604,050	450,000	22.50	333.3	480,000	352	506,199
Aug. 9	8:00 AM	22,424,024	25,535	20	21.3	30,642	2:00 PM	82,060,900	456,850	22.5	338.4	487,307	360	517,949
Aug. 10	8:30 AM	22,424,587	563	24.5	0.4	552	12:30 PM	82,475,700	414,800	22.5	307.3	442,453	308	443,005
Aug. 13	11:00 AM	22,426,950	2,363	26.5	1.5	2,140	8:00 AM	83,720,700	1,245,000	67.5	307.4	442,667	309	444,807
Aug. 14	12:30 PM	22,428,192	1,242	25.5	0.8	1,169	9:00 AM	84,117,800	397,100	25	264.7	381,216	266	382,385
Aug. 15							4:00 PM	84,555,000	437,200	31	235.1	338,477	235	338,477
Aug. 17	Pump Not Running													
Aug. 18							2:00 PM	85,145,000	590,000	70	140.5	202,286	140	202,286
Aug. 21							2:00 PM	86,323,887	1,178,887	72	272.9	392,962	273	392,962
Aug. 22	Pump Back Running													
Aug. 24	11:00 AM	22,454,200					11:00 AM	87,198,000	874,113	69	211.1	304,039	211	304,039
Aug. 27	11:30 AM	22,465,400	11,200	24.5	7.6	10,971	11:30 AM	88,042,500	844,500	72.5	194.1	279,559	202	290,530
Aug. 28	4:00 PM	22,466,000	600	28.5			4:30 PM	88,386,120	343,620	29	197.5	284,375	197	284,375
Aug. 29	29 Pump No. 1 Shut down for good at 8 AM													
Aug. 30							9:00 AM	88,575,509	189,389	16.5	191.3	275,475	191	275,475

Pump No. 2 Shut down for good at 9:00 AM Aug. 30

AVG 365,207

TABLE D-5 CLIMATIC WATER BUDGET: CLIMATE NORMAL 1981-2010 (Hanover) Potential Evapotranspiration Miramachi Shores Phase 4 Hydrogeological Evaluation Permit To Take Water (20007.00)

	Thornthwaite (1948)										
Month	Mean Temperature (°C)	Heat Index	Potential Evapo- transpiration (mm)	Daylight Correction Value	Adjusted Potential Evapo- transpiration (mm)	Total Precipitation (mm)	Surplus (mm)	Deficit (mm)			
January	-6.8	0.0	0.0	0.81	0.0	109.6	109.6	0.0			
February	-5.9	0.0	0.0	0.81	0.0	81.3	81.3	0.0			
March	-1.7	0.0	0.0	1.02	0.0	72.0	72.0	0.0			
April	5.8	1.3	27.9	1.12	31.3	73.1	41.8	0.0			
Мау	11.9	3.7	58.8	1.27	74.7	84.6	9.9	0.0			
June	17.2	6.5	86.2	1.29	111.2	78.3	0.0	32.9			
July	19.6	7.9	98.7	1.30	128.4	83.1	0.0	45.3			
August	18.6	7.3	93.5	1.20	112.2	95.0	0.0	17.2			
September	14.6	5.1	72.7	1.04	75.7	109.1	33.4	0.0			
October	8.4	2.2	41.0	0.95	39.0	89.7	50.7	0.0			
November December	2.6 -3.3	0.4 0.0	12.2 0.0	0.80 0.74	9.7 0.0	103.0 108.4	93.3 108.4	0.0 0.0			
TOTALS	6.8	34.3			582.2	1087.2	600.5	95.4			

TOTAL WATER SURPLUS 505.0

mm

NOTES:

1) Water budget adjusted for latitude and daylight.

2) (°C) - Represents calculated mean of daily temperatures for the month.

3) Precipitation and Temperature data from the Hanover Climatic Station latitude 44°06'59.058" N, longitude 80°00'21.042" W, elevation 270 masl

4) Total Water Surplus (Thornthwaite, 1948) is calculated as total precipitation minus adjusted potential evapotranspiration.